

AD-A169 538

CONVERSION OF THE NOLAPS (NAVY OPERATIONAL LOCAL
ATMOSPHERIC PREDICTION S. (U) RESEARCH AND DATA SYSTEMS
INC LANHAM-SEABROOK MD P ARDANUY FEB 86 NEPRF-CR-86-03

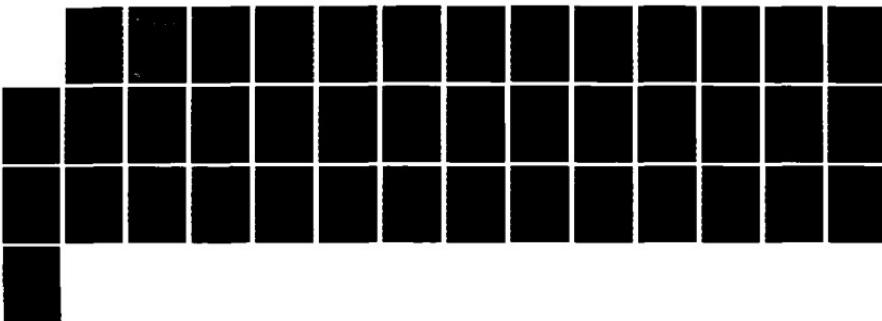
1/1

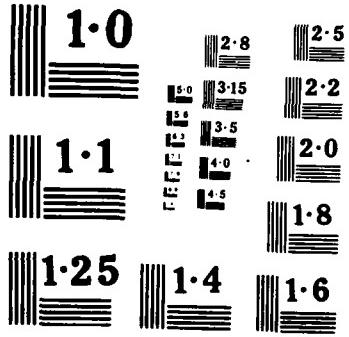
UNCLASSIFIED

N88228-84-D-3155

F/G 4/1

NL





12

NAVENVPREDRSCHFAC
CONTRACTOR REPORT
CR 86-03



CONVERSION OF THE NOLAPS MODEL TO THE HP9845

NAVENVPREDRSCHFAC CR 86-03

AD-A169 538

Philip Ardanuy

Research and Data Systems Corp.
Lanham, MD 20706

Contract No. N00228-84-D-3155

FEBRUARY 1986

DTIC ELECTE
S JUL 7 1986 D
B

DTIC FILE COPY

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION IS UNLIMITED

86 7 7 003

Prepared For:

NAVAL ENVIRONMENTAL PREDICTION RESEARCH FACILITY
MONTEREY, CALIFORNIA 93943-5006



QUALIFIED REQUESTORS MAY OBTAIN ADDITIONAL COPIES
FROM THE DEFENSE TECHNICAL INFORMATION CENTER.
ALL OTHERS SHOULD APPLY TO THE NATIONAL TECHNICAL
INFORMATION SERVICE.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE

AD-A169538

REPORT DOCUMENTATION PAGE

1a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED		1b. RESTRICTIVE MARKINGS	
2a. SECURITY CLASSIFICATION AUTHORITY		3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution is unlimited	
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE			
4. PERFORMING ORGANIZATION REPORT NUMBER(S)		5. MONITORING ORGANIZATION REPORT NUMBER(S) CR 86-03	
6a. NAME OF PERFORMING ORGANIZATION Research & Data Systems Corp.	6b. OFFICE SYMBOL (if applicable)	7a. NAME OF MONITORING ORGANIZATION Naval Environmental Prediction Research Facility	
6c. ADDRESS (City, State, and ZIP Code) 10300 Greenbelt Rd. Lanham, MD 20706		7b. ADDRESS (City, State, and ZIP Code) Monterey, CA 93943-5006	
8a. NAME OF FUNDING/SPONSORING ORGANIZATION Naval Air Systems Command	8b. OFFICE SYMBOL (if applicable) AIR-330	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER N00228-84-D-3155	
8c. ADDRESS (City, State, and ZIP Code) Department of the Navy Washington, DC 20361		10. SOURCE OF FUNDING NUMBERS	
		PROGRAM ELEMENT NO 62759N	PROJECT NO WF59-551
		TASK NO.	WORK UNIT ACCESSION NO DN656766
11. TITLE (Include Security Classification) Conversion of the NOLAPS Model to the HP9845 (U)			
12. PERSONAL AUTHOR(S) Ardanuy, Philip			
13a. TYPE OF REPORT Final	13b. TIME COVERED FROM 1/4/85 TO 11/4/85	14. DATE OF REPORT (Year, Month, Day) 1986, February	15. PAGE COUNT 36
16. SUPPLEMENTARY NOTATION See also companion publication CR86-04, Navy Over-Water Local Atmospheric Prediction System (NOWLAPS) Users Guide, February 1986.			
17. COSATI CODES		18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number) Higher order closure Turbulence Planetary boundary layer Refractivity Atmospheric modeling	
FIELD 04	GROUP 02		
04	01		
19. ABSTRACT (Continue on reverse if necessary and identify by block number) As a first effort in developing an atmospheric predictive capability for the Tactical Environmental Support System (TESS), the model used for the Navy Operational Local Atmospheric Prediction System (NOLAPS) is converted to the HP9845B, Option 275. Three primary steps are involved in this conversion. First, the model is converted from FORTRAN to BASIC code, made to duplicate existing model results, and benchmarked for time purposes. The converted model is renamed NOWLAPS (Navy Over-Water Local Atmospheric Prediction System). Second, a user-interactive capability is developed for this desk-top system. And third, an interactive graphics package is developed to display the model results.			
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT <input type="checkbox"/> DTIC USERS		21. ABSTRACT SECURITY CLASSIFICATION UNCLASSIFIED	
22a. NAME OF RESPONSIBLE INDIVIDUAL Dr. P. Tag, contract monitor		22b. TELEPHONE (Include Area Code) (408) 646-2927	22c. OFFICE SYMBOL WU 6.2-31BG

CONTENTS

1.	Introduction	1
1.1	Summary	1
1.2	Environment	1
1.3	Background	1
1.4	Statement of Work	3
2.	Task 1	5
2.1	Requirements	5
2.2	Code Conversion	6
2.3	Interactive Initialization	15
2.4	Restart Capability	16
2.5	Graphical Capability	16
2.6	Timing	17
2.7	Optimization	17
3.	Task 2	22
3.1	Requirements	22
3.2	CALSPAN Case 6	22
3.3	CALSPAN Case 3	22
4.	Task 3	25
4.1	Requirements	25
4.2	Final Report	25
4.3	User's Guide	25
4.4	BASIC Code Listing	25
5.	Conclusions	26
6.	Recommendations	27
6.1	Further Optimization	27
6.2	Enhancement of Capabilities	27
6.3	Further Testing	28
7.	References	29
7.1	System References	29
7.2	Model References	30
	Distribution	32

Note: Companion publication -- Navy Over-Water Local Atmospheric Prediction System (NOWLAPS) Users Guide -- published separately as NAVENVPREDRSCHFAC Contractor Report CR 86-04 dated February 1986.



1. Introduction

1.1 Summary

The purpose of this final report is to document the code conversion, testing, modification, benchmarking, and optimization of the Navy Operational Local Atmospheric Prediction System (NOLAPS), Planetary Boundary Layer (PBL), Higher Order Closure (HOC), turbulence model code for the HP9845 computer. The delivery order (QE-01) which encompasses this work is partitioned into 3 tasks, discussed in section 2 through 4, which respectively describe the code conversion procedure in full, the benchmarking procedure, and the final report.

1.2 Environment

As stated in contract N 00228-84-12-3155 "the Navy has plans to incorporate a mini-computer for environmental diagnosis and prediction onboard carriers and other selected ships and shore installations. This computer will be part of the Tactical Environmental Support System (TESS)." As a first step in developing an atmospheric prediction system for TESS, the NOLAPS turbulence model will be implemented into TESS and renamed NOWLAPS (Navy Over-Water Local Atmospheric Prediction System).* The eventual TESS computer will be a follow-on to the current-generation HP9845 A, and B option 275, shipboard microcomputers.

For this task, the NOLAPS HOC model is made operational on the current-generation HP 9845B microcomputer. Full advantage is taken in the revised model code of the capabilities of the HP machine, specifically special function key programmability, the two cassette drives, the in line printer, the graphics capabilities, and the screen-dump-to-printer feature.

1.3 Background

In an attempt to reduce the complexity of numerical models describing turbulent flow (following hypotheses of Kolmogoroff (1942), Prandt and Wieghardt (1945), Rotta (1951), and others), Mellor and Yamada (1974) of the Geophysical Fluid Dynamics Program at Princeton considered a set of systematic simplifications in the governing equations. This review led to the development of a hierarchy of

* Companion publication -- Navy Over-Water Local Atmospheric Prediction System (NOWLAPS) Users Guide -- published separately as NAVENVPREDRSCHFAC Contractor Report CR 86-04 dated February 1986.

turbulence closure models for the planetary boundary layer, with the set of models differing due to scaling considerations based on the degree of anisotropy permitted. An intermediate, so-called "level-3" model was identified as comprising an optimal combination of reduced computational complexity (only two of the ten differential equations of the higher level-4 model are retained) and desirable solution characteristics (numerical experiments (Yamada and Mellor, 1975) indicated that both models produced practically the same results). This level-3 model was first described by Mellor (1973); Yamada and Mellor (1975) have given a full treatment of the numerical procedures involved in the time integration of the model's equations and discuss in detail comparisons of prognostic results with observations.

Following the authors' closure assumptions for the triple turbulence moments and the scaling considerations implicit in the derivation of the level-3 framework, the model requires the solution of the finite difference analogs of the partial differential equations for the total turbulent kinetic energy and potential temperature variance, mean velocity and temperature. The remaining turbulent moments are obtained through the simultaneous solution of a derived set of algebraic equations.

Using a higher-order turbulence closure model similar to the level-3 model developed by Mellor (1973) and Mellor and Yamada (1974), Burk (1977) of the National Severe Storms Laboratory at NOAA investigated the temporal behavior of moisture stratification within the diurnally-varying planetary boundary layer (PBL). Because the computation of moisture-related fluxes was of prime concern, numerical solution of the partial differential equations for the temperature-moisture covariance and the specific humidity variance, rather than the less-complex algebraic equation subsets, was incorporated into the numerical model. Application of appropriate initial and boundary conditions to this one-dimensional model then allowed the time-dependent solution of the spatial variation of the mean horizontal wind components, virtual potential temperature and specific humidity, as well as related variables. Following a linear stability analysis which showed that the finite difference expression utilized by Yamada and Mellor (1975) failed under conditions of large stability, Burk (1977) redefined the expressions for this case.

Burk and Thompson (1982), of the Naval Environmental Prediction Research Facility (NEPRF) at Monterey, took the level-3, second-moment closure turbulence model discussed in the preceding paragraph, coupled in estimates of atmospheric refractivity characteristics (Burk, 1980), detailed cloud physics as developed by Sommeria and Deardorff (1977) and Mellor (1977), the precipitation parameterization of Barker (1977), and a detailed solution of the radiative transfer equations (both in-cloud and out) as developed by Oliver et al. (1978). The model is initialized either solely with large-scale field information (e.g., interpolations to the PBL model grid of standard-level values from the FNOC primitive equation (PE) model, or based on any designated ship sounding available from the FNOC global database. Similarity-theory solutions yield variables at the model's lower boundary; all turbulence variables are set to zero at the top of the model's grid (e.g., 3.75 km) and the wind, temperature, and moisture gradients are specified. After obtaining an initial state in the wind, temperature, and moisture fields, a dynamic initialization is effected. This "spin-up" procedure holds fixed the mean fields as the turbulence variables interactively evolve to a near-equilibrium state. At this point, the model begins its forecast and the mean fields are permitted to change. In order to incorporate into the forecast synoptic changes occurring at the location of the boundary layer forecast, total time derivatives of the large-scale variables based on the FNOC PE model forecast are interpolated to the PBL grid and added to the mean PBL equations. Through the use of altitude-dependent weights, forecasts are obtained in which the high-resolution closure model terms dominate in the boundary layer, while the 12 and 24 hour large-scale PE model forecasts are reproduced above 850 mb. The result is an operational forecast system designed to provide high-resolution boundary-layer forecasts based on any specified ship sounding, bulk air-sea differences, and large-scale wind and tendency terms (Burk and Thompson, 1982). The useful output products of this forecast system include, to name a few: fog and visibility forecasts, boundary layer winds and atmospheric refractivity characteristics.

1.4 Statement of Work

As specified in the Statement of Work for Contract N00228-84-D-3155, Delivery Order QE-01 there are three tasks:

1.4.1

Task 1

The contractor shall become familiar with the NEPRF one-dimensional HOC model and the HP9845B, Option 275 microcomputer. If the contractor does not have access to an HP machine, off-hour and a limited amount of working hour time will be provided on the NEPRF HP9845B, Option 275. NEPRF will provide FORTRAN code for the HOC model. Because interpreted BASIC is the primary language for the HP9845, the contractor shall convert the HOC FORTRAN code into BASIC code for the HP9845. The contractor shall then segment, optimize, or otherwise manipulate this BASIC code into a program runnable on the HP9845B, Option 275. In addition, the contractor shall streamline the model's input and output into a form compatible with the HP machine. Specific goals regarding this program conversion are defined in the section entitled "Requirements." A minimum of two letter progress reports shall be submitted during this phase of work.

1.4.2

Task 2

Having converted the HOC model into BASIC code and adapted this code to the HP machine, the contractor shall run a minimum of two HP HOC (to be defined by the COTR) runs for comparison to mainframe benchmarks. The contractor shall show that the HP model results are identical to the mainframe results. A letter progress report shall follow Task 2.

1.4.3

Task 3

The contractor shall write a report detailing and documenting all of the steps necessary to achieve Tasks 1 and 2. This report shall include a specific section which describes in detail the input, running and output procedures for the converted model. Specific recommendations regarding potential additional speed enhancements shall be made in this report.

2. Task 1

2.1 Requirements

As specified in the Statement of Work for Contract N0028-84-D-3155, Delivery Order QE-01 the requirements for Task 1.1 are:

2.1.1 Code Conversion and Optimization

The benchmark running time goal for running the HOC model on the HP9845B, Option 275 is one hour for a 24 hr. forecast. This one hour running time is wall time, starting after the model is initialized with meteorological input data and ending with the forecast products output from the model. Based on CDC 6500/HP9845B, Option 275 benchmarks of comparable code, the one hour benchmark should be realizable. In the event that the contractor cannot achieve this benchmark during the course of the contract, the contractor shall detail to the contract monitor the reasons for failure, as well as extreme measures that might be taken to achieve the benchmark. Following initial conversion and running of the model on the HP machine, the contractor shall report to the contract monitor the running speed. In the event that the initial HP version results in a running time of less than or equal to one hour, the contractor shall optimize the code so as to decrease the running time 20%. In the event that the contractor cannot meet this benchmark, the same procedure as above shall be followed.

2.1.2 Code Conformance

Because the fleet HP computers are cassette-based, the HOC model shall be completely tape oriented. Optimizations to the HOC code shall be optimizations in BASIC code only (one command per one line); no assembly code is to be used. This BASIC code shall conform to the "NEPRF BASIC Code Standard" (to be published). Further, any optimizations are to be coded optimizations only; there are to be no changes in the HOC model physics, resolution, or time step.

2.1.3 Interactive Initialization

The HP HOC model will be designed to be initialized from the HP keyboard. The contractor shall design the initialization so that the user is prompted for all input data. This initialization procedure will be designed such that default data is easily utilized.

2.1.4 Standard Model Output and Restart

All standard model output will be written to CRT, and optionally to hard copy, during the course of the model's run (e.g., the output valid halfway through the run will be written at that time). The specified interval of output will be defined in the prompted initialization. In addition to this hard copy output, the program shall be designed to output data to cassette tape for restart purposes. The program shall have the capability to restart from any of these cassette output times; the model results from either a restart or a continuous run shall be identical. A header (prologue) will be displayed as the header code is loaded from tape (see Figure 1).

2.2 Code Conversion

Code conversion of the NOLAPS model was undertaken in 3 segments: (1) translation of the model dynamics from FORTRAN to BASIC; (2) development of an interactive framework for easy user interface; (3) installation of a graphics capability to facilitate user diagnosis of the forecast. The latter 2 segments are detailed in sections 2.3 - 2.5. Subject to the requirement that the model physics not be altered, and the requirement (section 3) that benchmark tests be performed and passed, care was taken to insure that an exact code translation was achieved. Whenever expedient, however, structured programming was used by taking full advantage of the structured programming ROM available in the HP9845. In addition, substantial optimization of the model code was performed at this juncture to reduce the need for later passes through the program (see section 2.7). The "Programming Guide for Shipboard Numerical Aid Programs" (Brown, 1984) was adhered to for guidance on general and detailed requirements, as well as "human factors" consideration. Some examples of this are listed below.

NAVY OVER-WATER LOCAL ATMOSPHERIC PREDICTION SYSTEM (NOWLAPS)
(A ONE DIMENSIONAL BOUNDARY LAYER PROGNOSTIC MODEL)

WRITTEN BY:
DR. STEPHEN D. BURK
AND MR. WILLIAM T. THOMPSON

ADAPTED TO THE HP9845B, OPT 275 BY:
DR. PAUL M. TAG
AND RESEARCH AND DATA SYSTEMS, CORP.

NAVAL ENVIRONMENTAL PREDICTION RESEARCH FACILITY
MONTEREY, CALIFORNIA 93943-5006
(408) 646-2927
DEVELOPED IN HP-BASIC FOR THE :
SHIPBOARD NUMERICAL AID PROGRAM

REFERENCE: THE NOWLAPS USER'S GUIDE
LAST REVITION: JANUARY 13, 1986
PROGRAM NOW LOADING

Figure 1. NOWLAPS Prologue

2.2.1 Entry-Exit Structure

Each program segment has only one entry and exit. This limitation necessitated individual functions CORWS and CORWL, unlike the FORTRAN counterparts.

2.2.2 Size

Whenever possible, the subprograms were limited to less than 100 executable statements. For clarity, however, conformance of the program structure was kept identical to the FORTRAN counterpart as much as possible. The functions of the resultant subprograms are summarized briefly in Table 1 and their flow illustrated in Figure 2.

2.2.3 Indentation

Indentation of program statements was universally applied, except for those read-from-tape statements that would then have exceeded the line length restriction and been truncated. (The structured programming ROM does truncate these statements when its indentation utility is used. The statements must then be manually restored.)

2.2.4 Naming

Naming conventions are universal throughout the model code. This is facilitated by the use of labelled common containing the global variables.

2.2.5 Constants

Constants were determined identically with the FORTRAN code in order to meet the mainframe benchmarks.

2.2.6 Significant Digits

Full precision model variables were employed throughout the program.

2.2.7 Abstracts

Detailed textual abstracts are provided at the beginning of the executable coding for the main program and each subprogram.

TABLE 1
Subprogram Names and Functions

AUTOST	This subroutine writes a prologue, loads the softkeys, and loads the program.
BCS	This subroutine inserts the upper and lower boundary conditions for the turbulence variables, calls subroutine THOMAS, and stores the newly-calculated turbulence variables. This subroutine was formerly part of the MAIN program in the FORTRAN version of program CLOSURE.
BOUND	This subroutine calculates the Louis/ECMWF drag coefficient and the Monin-Obukhov length for the stable, neutral, or unstable PBL. It then calculates the surface layer fluxes of momentum, heat, and moisture using the newly-calculated drag coefficients.
CHAREN	This subroutine accepts only single-character input from the user during an interactive session; i.e., Y or N for a yes or no query.
CLEARSS	This subroutine clears the screen.
COEF	This subroutine calculates the coefficients for the general tridiagonal matrix before the boundary conditions have been inserted.
CORCR	This subroutine calculates the path integrals and then the downward transmissivities.
CORRD	This subroutine defines the radiative constants and variables used in CORCR.
DEW	This subroutine accepts numerical input for the dew point or dew point depression from the user during an interactive session.
ENTERS	This subroutine accepts numerical input from the user during an interactive session.
ESAT	This subroutine computes the saturation vapor pressure of the air using a 6th order polynomial expansion when given the temperature in degrees Kelvin.
FCST	This subroutine initiates the forecast.
FNCORWL	This subroutine calculates the total transmissivity for the longwave radiation.
FNOORWS	This subroutine calculates the total transmissivity for the shortwave radiation. This was formerly part of

CORWL in the FORTRAN version CLOSURE.

GRAPH	This subroutine produces graphical displays and diagnosis of the NOLAPS forecast.
GREEN	This subroutine accepts user entry of Greenwich Mean Time and converts to useable form.
HEADER	This subroutine determines whether a new sounding will be defined or a previously-entered sounding, stored in the header record, will be used to make a forecast.
HEIGHT	This subroutine accepts numerical input for Height, from the user during an interactive session.
HICHEK	This subroutine verifies that the data extends above the top of model grid.
HIST	This subroutine creates a history record.
HOSKEEP	This subroutine calculates the eddy momentum coefficient, the eddy heat coefficient, and the liquid-water-related variables.
INITIAL	This subroutine specifies the initial lower boundary values. It calculates factors used in computing derivatives and calculates the initial M-Y length scales. This subroutine was formerly lines 75 to 135 of the main program in the FORTRAN version of program CLOSURE.
INVAR	This subroutine sets up the initial conditions for numerous variables. INVAR was formerly subroutine INITIAL in the FORTRAN version of program CLOSURE.
ITER	This subroutine is used both for the dynamic initialization and to forecast. ITER was formerly lines 136 to 473 of the main program in the FORTRAN version of program CLOSURE.
LSCALE	This subroutine defines a weight factor that operates on the large-scale tendencies. LSCALE was formerly lines 424 to 448 of the main program in the FORTRAN version of program CLOSURE.
LSTEND	This subroutine accepts a value for the time that the next set of large scale (L/S) tendencies are to be read. It then accepts the values to be stored as the set of L/S tendencies. All values are entered by the user during an interactive session.
MAIN	Main routine which oversees the running of the NOLAPS program.

MEANS	This subroutine calculates the new U and V components for the mean wind. It then determines if radiation should be computed for this time step, and if so, calls CORRD. Finally, it computes the new mean values of the virtual potential temperature and the specific humidity.
MTAPE	This subroutine reads the header and history records from the history tape.
QLT	This subroutine prints out all the important variables of the forecast at set time intervals.
XTP	This subroutine prints out all the data that was entered during the interactive session.
PARAM	This subroutine allows the user to select one of two predefined grids.
PRESS	This subroutine accepts numerical input for the pressure during an interactive session.
SETUP	This subroutine initializes all the constants used throughout the program. SETUP also initializes certain string arrays with the dialogue needed for the interactive session.
SITEND	This subroutine calls subroutine ENTERS to accept numerical input from the user during an interactive session. This input is stored either in the array for the site variables or the array for the large-scale tendencies.
SOUND	This subroutine initiates the interactive session. It guides the user through each step with the aid of prompts, waits for replies, and issues error messages when appropriate. It allows the user to set up new run parameters and enter site variable, large-scale-tendencies, the temperature sounding, and the wind sounding. The user can also back up to any previous entry to make a change.
SPINUP	This subroutine initiates the dynamic initialization.
STRETCH	This subroutine calculates the grid to be used in the forecast.
TEMPS	This subroutine is the part of the interactive session which allows the user to enter data for a temperature sounding. This data consists of temperature, height, dew point or dew point depression, and pressure.

TEND	This subroutine determines which set of large scale tendencies will be interpolated to the grid and does the interpolation. TEND was formerly lines 158 through 185 of the main program of the FORTRAN version of program CLOSURE.
THOMAS	This subroutine solves the tridiagonal set of equations which includes the boundary conditions via the Thomas algorithm.
THOMASF	This subroutine solves the tridiagonal set of equations with flux boundary conditions via the Thomas algorithm.
UVCOMP	This subroutine sets up the boundary conditions and solves the tridiagonal set of equations which yield the new U or V component for the mean wind.
WINDS	This subroutine is the part of the interactive set of code which allows the user to enter data for a wind sounding. This data consists of either the U and V components of the wind, or the speed and direction.
VINTRP	This subroutine linearly interpolates or extrapolates to obtain variables at the height of the grid points using, as input, values of the points obtained from the sounding.

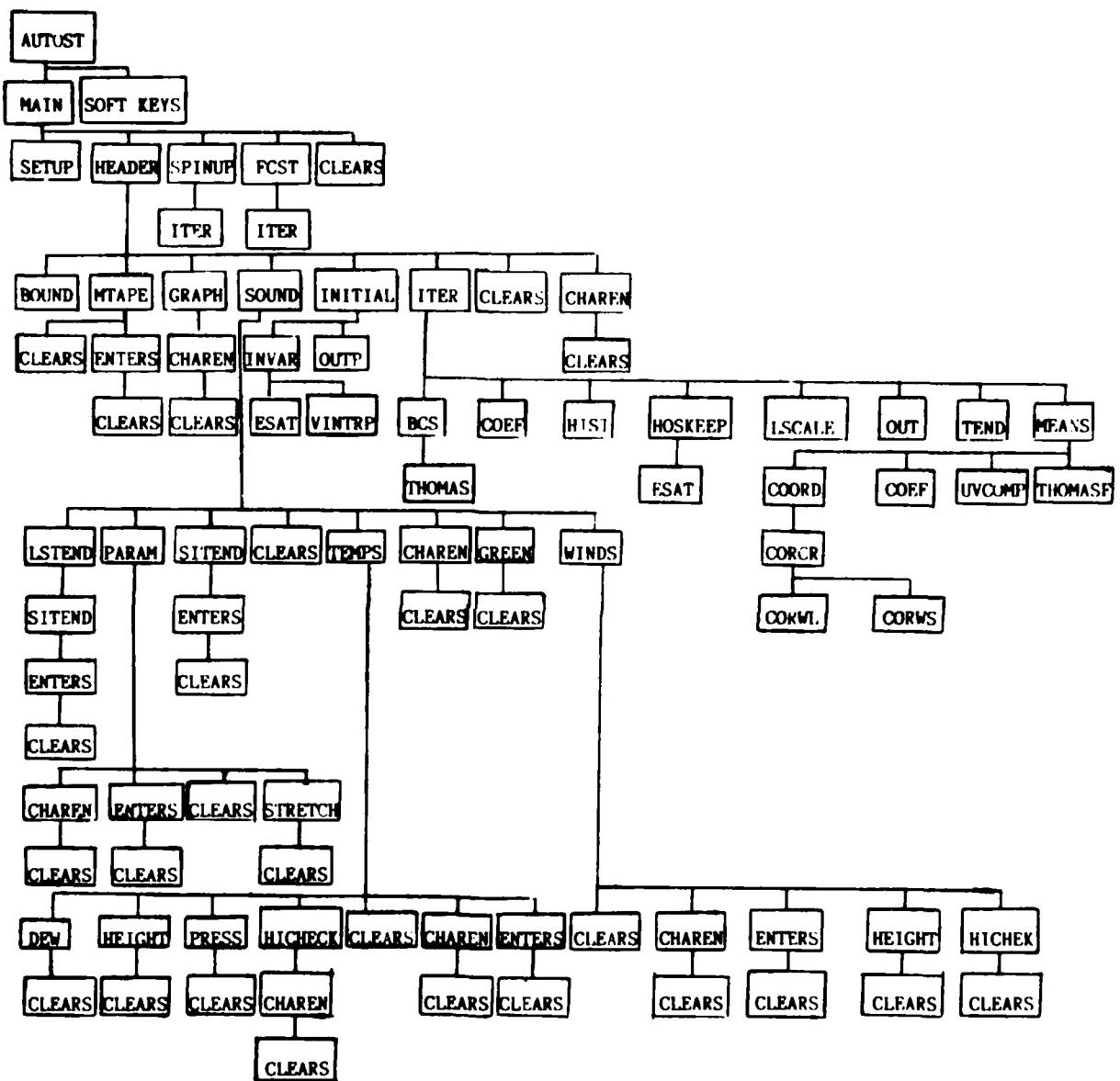


Figure 2. Hierarchy chart of the NOWLAPS subprograms.

2.2.8 Comments

Comments are used throughout the code.

2.2.9 Labels

With several exceptions, line numbers, rather than line labels, are used in program branches. One notable exception is in the OPTION branch for special function key number 1.

2.2.10 Labelled Common

Comments are used to distinguish between different common blocks. In general, variables are grouped in common blocks labelled by that routine name within which they were first defined.

2.2.11 Data Statements

Program constants, as defined in data statements, are all now located in the static initialization portion of the code.

2.2.12 Abnormal Termination

System errors are trapped using ON ERROR statements. These conditions are possible when manipulations of the history tape files are performed. The code is designed to correct the error conditions.

2.2.13 Units

Units are generally MKS. Exceptions are made in those extensive computations for which the FORTRAN code used units other than MKS. For consistency, the unit conventions are maintained.

2.2.14 Special Function Keys

Special Function Key (SFK) definitions are consistent with the NEPRF standards (Brown, 1984).

2.2.15 Program Overlays

No program overlays are required or used.

2.2.16 Default Values

Where appropriate, default values are displayed for the convenience

of the user. To avoid the loss of data when the user is "backing up," the previous answer to the question becomes the new default.

2.2.17 Feedback

All user entries are echoed.

2.2.18 Data Entry

The data entry process guidelines are followed.

- o program displays a prompt
- o user enters information
- o program echoes the entry on the screen
- o program error checks the entry
- o program displays an error message
- o information is edited as needed
- o information is accepted

2.2.19 Prompting

As shown in the example in the User's Guide, the entry format guidelines are followed exactly.

2.2.20 Editing

The user may edit entries at more than one stage: during initial entry, after a block of related entries have been made (by "backing up"), and after the data have become part of a data base (by reading the header record on the history tape and then modifying and recreating the data).

2.3 Interactive Initialization

A comprehensive and carefully constructed capability exists to facilitate the entry or revision of the initial state for a model forecast. Defaults are displayed where appropriate, including hypsometric estimates of pressure, given height, temperature, and dewpoint temperature. The user is able to back up to revise previous answers. Upon backing up, previous answers to questions become the new default values. The user is guided, step by step, through the entire set of parameters requisite to a forecast. For flexibility, either wind

direction and speed or the U and V wind components may be entered. Similarly, either the dew point temperatures or the dew point depressions may be entered. It is possible for the user to bypass the entire block of questions regarding the large scale tendencies if none are to be specified. The User's Guide covers the details of this interactive, static initialization.

2.4 Restart Capability

The capability exists for restarting an interrupted forecast at several points in the process:

- o at the end of the static initialization, when all the initial state data has been inserted and a header record written to tape;
- o at the end of the dynamic initialization, when the model's "spin up" is completed, and the "zero'th" history record has been written to tape; and,
- o at any of the model's output intervals, when the history records have been written to tape.

The user is also given the opportunity of modifying a previous initial state (header record) if this is desired. The logic contained in the restart portion of the code is described fully in the User's Guide.

As required, the model predictions from a continuous and a restart run are identical. All variables that are not re-initialized by the model code in an interaction prior to use are stored on tape. Since full precision variables are stored exactly on tape, no loss of accuracy occurs.

2.5 Graphical Display

The interactive BASIC NOWLAPS code has the ability to diagnose the forecast for any history record written to tape. Both figures and tabular output may be obtained. The method of user access is discussed in the User's Guide. These capabilities are available to the user at any time before, during, or following model execution by simply

depressing KEY 1 to go to label OPTION, or by appropriately answering the program queries.

2.6 Timing

A timing test was performed on the translated NOLAPS model code. For these tests, a HP9845 option 175 was used. It should be noted that execution times of math floating point routines in the option 275 computer are typically 5 times faster than in the comparable 175 machine (See Table 2). The data set was the so-called CALSPAN case-3 benchmark, as provided by NEPRF (see Mack, et al., 1983). Case 3 is an 18 hr. (222 time step) fog/stratus simulation. Using the case-3 input data, the following running times (per time step) were measured:

5.4 seconds: no radiation

8.7 seconds: longwave radiation only (night)

12.9 seconds: longwave & shortwave radiation (day).

The total forecast took 48 minutes and 40 seconds. This timing included 7 output intervals, each with a write to screen time of approximately 32 seconds and a write to tape time of approximately 20 seconds. The 7 output intervals thus consumed approximately 6 minutes and 4 seconds. By removing this time from the total time, a 24-hour forecast time can be extrapolated to be 56 minutes and 48 seconds. Because two of the output intervals are forecast requirements (at the end of the dynamic initialization and at the end of the forecast), this time must be added to the forecast time to yield an effective total forecast wall clock time length of 58 minutes and 32 seconds. This timing is consistent with the 1 hour wall clock time goal as stated in the requirements. Of course, the exact wall clock time of the forecast will depend on the number of calls to radiation (every time step when liquid water is present) and the length of the daylight portion of a 24-hour forecast.

2.7 Optimization

Further optimization of the NOLAPS BASIC code was initiated at this time, the goal being a further reduction in the wall clock time

Table 2

Timing Comparisons for the HP9845, options 175 and 275.

Routine ¹	Time (ms)	
	Opt. 175	Opts. 275,280
Addition	0.27	0.04
Subtraction	0.33	0.06
Multiplication	0.89	0.14
Division	2.90	0.56
Raise to power	17.00	3.21
Square root	2.90	0.43
Tangent	14.00	2.41
Sine	21.00	3.68
Cosine	21.00	3.68
Arctangent	18.00	2.31
Arcsine	26.00	3.88
Arcosine	26.00	4.00
Natural log	7.50	1.39
Log base 10	9.70	1.49
e ^x	6.10	1.00
Integer	0.46	0.24
Absolute value	0.13	0.03
Fraction	0.35	0.09
Random number	1.80	0.33

¹ Based on a table provided in the HP 9845 Computer Family Specifications, P2.

length of a forecast. The optimization variables were installed in a common block called /OPTIM/. Specific improvements involved precomputing a set of composite denominators relating to vertical gradients, removing data reads from the radiation package, and precomputing the spherical trigonometry/ law of cosines terms necessary for the solar zenith angle. It was verified that runs made with these changes produced identical results with the pre-optimization benchmark case-6 reference.

A retiming of the model runs following these changes showed an optimization of 4%. (This improvement is in addition to those time savings resulting from revisions already performed at the time of the original code translation.) For example, the daytime calculations took 12.3 seconds/time steps, reduced from the previous length of 12.9 seconds by approximately 4%.

Following this optimization, final timing tests were conducted. Data from the CALSPAN case-3 benchmark were utilized and two runs were made. In the first, data with a single asterisk (see Tables 3 and 4) were used to form the vertically-interpolated, 25 point, 2250 meter initial state. In the second run, data with single and double asterisks were used. Data without any asterisks were excluded from the vertical interpolations for these comparisons only. (The benchmark accuracy comparisons with NEPRF-supplied mainframe results used all the data). The difference between the two runs is that, following the vertical interpolation in the static initialization, no cloud will exist in the former run. This comparison is important since the radiation is computed every time step when liquid water is present in the model grid, yet only every six timesteps when no liquid water is present.

As expected, the first run was substantially quicker than the second. With output intervals following only the dynamic initialization and the full 24-hour forecast, the wall clock times were:

<u>Run</u>	<u>Time (minutes:seconds)</u>
1 (no cloud)	28:52
2 (with cloud)	50:35

TABLE 3
Initializing thermodynamic data from CALSPAN case 3 benchmark

Sounding level	Pressure (mb)	Temperature (°C)	Dewpoint depression (°C)	Height (m)
Temperature Sounding				
* 1	1012	17.6	01.3	4
**2	996	16.1	00.0	144
**3	982	15.3	00.0	265
**4	977	15.5	08.1	305
* 5	974	21.1	23.1	335
6	971	23.3	24.8	361
7	965	25.1	25.1	415
8	938	25.7	25.3	664
9	927	25.1	25.1	768
10	895	23.3	24.8	1075
11	871	21.7	24.9	1311
12	861	21.2	24.5	1411
* 13	850	20.4	24.3	1522
14	700	9.6	22.4	3151
15	500	-5.6	30.0	5875
* 16	400	-20.1	30.0	7580
17	300	-36.9	30.0	9641
18	200	-56.8	30.0	12319
* 19	100	-73.4	30.0	16494

TABLE 4
Initializing momentum data from CALSPAN case 3 benchmark

Sounding level	U component (m/sec)	V component (m/sec)	Height (m)
Wind Sounding			
* 1	3.0	0.0	5
* 2	-0.1	-2.1	400
* 3	-3.9	-5.6	1500
* 4	-3.9	-5.6	3000

It is significant that the second run's timing is less than the 24 hour estimate of 56:48, which was based on an extrapolation of the 18 hour forecast to 24 hours (with a factor of 4/3). This difference relates to the 1100 GMT start time, for which the full daylight period (with correspondingly longer time steps) is contained in the first 18 hours of the forecast. It is therefore incorrect to extrapolate these daylight timesteps into what would otherwise have been night if the forecast had been allowed to continue.

3. Task 2

3.1 Requirements

As specified in the Statement of Work for Contract N00228-84-D-3155, Delivery Order QE-01, the requirements for Task 2 state:

The contractor shall ensure that the results of the HP HOC runs agree with the mainframe benchmarks to within four significant digits. This agreement shall be demonstrated for the restart capability also.

3.2 CALSPAN Case 6

The CALSPAN case 6 benchmark run used the standard model code for a (220 minute, 43 iteration) forecast. CALSPAN case 6 was a stratus lowering to Fog case over cold water (Mack et al., 1983). It was necessary to use Teten's formula of water vapor pressure for this comparison as the original polynominal expansion was not accurately evaluated in the HP 9845. This switch to Teten's formula was determined to be necessary due to the inherent inability of the HP9845 to accurately replicate vapor pressures computed on the FNOC mainframe using the polynomial method. This inability was presumably due to an accuracy requirement in the polynomial evaluation beyond the capabilities of the HP9845. When Teten's formula was substituted, consistent estimates were obtained by the two systems. This, however, is not the delivered version which instead contains the polynomial representation. With this alternative version of the vapor pressure subroutine, the requisite four significant places of accuracy in all model variables were exceeded, even for the liquid water specific humidity (QL) and the cloud fraction (RC) which have proven to be among the most sensitive parameters. Complete sets of the BASIC model and the benchmark model output for all model output intervals were provided to the OOTR at the time of verification.

3.3 CALSPAN Case 3

Because the CALSPAN case 3 benchmark required revisions to the standard model code, particularly in the areas of sea surface temperature time dependence and the vertical structure of large-scale subsidence. These revisions resulted in comparison discrepancies

against the mainframe benchmark which were initially attributed, incorrectly, to errors in the model logic itself. These discrepancies did delay Task 2 until the errors were correctly trapped and removed. When the code was running properly, a successful 246 time step (20 hour) benchmark comparison was made. The results are detailed below.

The run used Teten's formula in the computation of the vapor pressure in subroutine ESAT, and was followed up with a forecast using the original polynomial expansion. For the former run, using Teten's formula, all variables agreed to a high degree of accuracy at time step 10, but the accuracy fell off slowly as time progressed. It is impossible to make any statement about error growth between timesteps 10 and 126 as we have no comparison data for that period. By time step 126, the U field is comparatively accurate to 4-5 places in the boundary layer (PBL) and to all 9 places listed above the PBL. Similarly, the V field shows an accuracy of 4 places in the boundary layer and 9+ places above, with the exception of the first layer where only 3 accurate digits are obtained. This first-layer inaccuracy is no doubt due to the fact that the wind component is relatively weak at that level and thus has the same absolute accuracy as the higher levels. The liquid water virtual potential temperature, or THL (the third prognostic variable), appears accurate to all 6 places provided in the NEPRF printout, while the total water substance specific humidity, or QW, behaves similarly in accuracy to the U component of the wind. The cloud fraction, a relatively sensitive parameter, shows an accuracy of from 3 to 4 digits, or to at least .03% in "cloud" units. By time step 246, some additional degradation in forecast accuracy is realized. For the winds, the U and V components are accurate to 5 and 4 digits, respectively, in the boundary layer, with an additional loss of 1 more digit in the V component whenever the velocity components fall an "order of magnitude" below the values (-09.692E-1 vs. -01.07916E0) of the other levels; both components have an accuracy, however, of the order of ten thousandths of a m/sec. The variable THL is accurate to 5-6 places in the boundary later and better above, while the variable QW shows an accuracy of 4 places in the boundary layer and better above. The cloud variables QL and RC are less accurate, with the cloud amounts for example correct

only to the tenth's of a percent (eg., .058 vs. .06, .461 vs. .463, .6419 vs. .6422, .5677 vs. .5683). All the cloud layers are predicted correctly as are the layers with 100% cloud. The losses in accuracy reviewed above appear to be simply the result of nonlinear error propagation during the course of the forecast due to the precision differences between the two machines, and thus not amenable to further improvement. As with the case 6 benchmark, complete sets of BASIC model and benchmark model output for all model output intervals were provided to the COTR at the time of verification.

4. Task 3

4.1 Requirements

As specified in the Statement of Work for Contract N00228-84-D-3155, Delivery Order QE-01 the requirements for Task 3 state:

The contractor shall provide two HP cassettes, each containing the HP HCC BASIC code. The contractor shall provide one camera-ready original plus two copies of the final report. Separately, the contractor shall provide three copies of the HCC model in BASIC code. This code shall be presented in a one statement per one line format and shall include comments or other documentation detailing changes or manipulations of the original HCC FORTRAN code. The report shall include a specific section which describes in detail the input, running, and output procedures for the converted model.

4.2 Final Report

This document constitutes the final report for this delivery order.

4.3 User's Guide

A user's guide to the NOLAPS model code is included with the final report.

4.4 BASIC Code Listing

Three copies of the fully documented BASIC code listing of the NOLAPS code are included with this final report.

5. Conclusions

As stated in the previous sections, the goals of Tasks 1, 2, and 3 have been achieved. The model code, as developed, has been demonstrated:

- o to function correctly, relative to the 2 required benchmark runs.
- o to restart correctly, relative to a continuous run.
- o to provide graphical forecast diagnosis.
- o to permit interactive static initialization.
- o to be well documented internally, and externally via a model user's guide, and
- o to be constructed in a "user-friendly" manner, so as to facilitate interaction.

6. Recommendations

6.1 Further Optimization

- a) It has been demonstrated that including radiation computations adds from 61% to 139% extra wall clock time to the length of each time step (section 2.6) depending on the solar zenith angle. As such, the radiative transfer portion of the code is one area for which further optimization may significantly reduce the time length of a forecast. These optimizations could be numerical approximations, for example utilizing simple lookup tables to replace calls to exponential functions.
- b) It has been demonstrated (section 2.7) that the presence of liquid water will almost double the length of wall clock time required to complete a forecast. This doubling results from radiation being called every time step when liquid water is present. This requirement may be unnecessary and should be critically examined.

c) The execution time of the model, and the amount of tape storage of the code, may be significantly reduced by stripping off the extensive internal documentation.

6.2 Enhancement of Capabilities

- a) During a forecast diagnosis (sections 2.5 and 8.5) the number of variables that may be examined is somewhat less than the number included in the standard model output at each output interval. Tape length limitations restrict the amount of data written to tape at each output interval to be that minimum amount needed to perform a restart (for plotting purposes, the modified index of refraction and the dew point temperature are derived from other variables). If a full set of output is desired, the model will have to make a one time step forecast, possibly with the large-scale variables held constant as during spin up. This procedure would allow the many temporary, or diagnostic, variables to be computed; they are not written to the history tape to save space. This capability would require code changes to the existing software.

b) In the plot of the modified index of refraction, ducting layers are shown graphically. It would be possible to incorporate a similar feature, in the temperature and dew point temperature plots, to represent cloud layers.

6.3 Further Testing

a) No tests have been conducted relative to the two benchmark cases with nonzero large-scale (L/S) tendencies. A third benchmark test should be conducted in the future to check out the L/S tendency terms and logic as it exists.

7. References

The following documents are references for this project:

7.1 System References

1. SECNAVINST 3560.1 Navy Tactical Digital Systems Documentation Standards.
2. MIL-STD-1679 (Navy) Weapon System Software Development, 1 December 1978.
3. TESS Tactical Operational Requirement (TOR)-Oct. 1981.
4. TESS System Operational Specifications (SOS)-Sept. 1982.
5. Navy Operational Local Atmospheric Prediction System (NOLAPS): Users Manual, NAVENVPREDRSCHFAC Document No. 7W0513 UM-12, 1983.
6. BASIC Programming for the HP 9845: September 1981, Hewlett Packard Part No. 09845-93000, 3003 Scott Blvd., Santa Clara, CA 95050, 267 pp. BASIC programming for the HP9845 Hewlett Packard Part No. 09845-93000.
7. Hewlett Packard System 45B Desktop Computer Operating and Programming Manual, 3003 Scott Blvd., Santa Clara, CA 95050, 267 pp.
8. HP 9845 Computer Family Specifications, Technical Data: February 1982, Hewlett Packard Part No. 5953-4603, 3003 Scott Blvd., Santa Clara CA 95050, 12 pp.
9. Brown, T., 1984: Programming Guide for Shipboard Numerical Aid Programs (SNAP). Naval Environmental Prediction Research Facility TR 84-06, Monterey, CA 92943-5006, 20 pp.

7.2 Model References

1. Burk, S.D., and W.T. Thompson, 1982: Operational evaluation of a turbulence closure model forecast system. Mon. Wea. Rev., 110, 1535 -1543.
2. Kolmogoroff, A.N., 1942: The equations of turbulent motion in an incompressible fluid. Izv. Akad. Nauk SSSR Ser. Fiz., 6, No. 1, 2, 56-58.
3. Mack, E.J., C.W. Rogers, and B.J. Wattle, 1983: An evaluation of marine fog forecast concepts and a preliminary design for a marine obscuration forecast system. CALSPAN report No. 6866-M-1.
4. Mellor, G.L., 1973: Analytic prediction of the properties of stratified planetary surface layers J. Atmos. Sci., 30, 1061-1069.
5. _____, and T. Yamada, 1974: A hierarchy of turbulence closure models for planetary boundary layer. J. Atmos. Sci., 31, 1791-1806.
6. _____, 1977: The Gaussian cloud model relations. J. Atmos. Sci., 34, 356-358.
7. Oliver, D.A., W.S. Lewellen and G.G. Williamson, 1978: The interaction between turbulent and radiative transport in the development of fog and low-level stratus. J. Atmos. Sci., 35, 301-316.
8. Prandtl, L., and K. Wieghardt, 1945: Ueber ein neues formel system fur die ausgebildete turbulence. Nachr. Akad. Wiss., Gottingen, Math. - Phys. Kl., 6-19.

9. Rotta, J.C., 1951: Statistische Theorie nichthomogener Turbulenz. Z. Phys., 129, 547-572; 131. 51-77.
10. Sommeria, G. and J.W. Deardorff, 1977: Subgrid-scale condensation in models of nonprecipitating clouds. J. Atmos. Sci., 34, 344-355.
11. Yamada, T., and G. Mellor, 1975: A simulation of the Wangara atmospheric boundary layer data. J. Atmos. Sci., 32, 2309-2329.

DISTRIBUTION

COMMANDER IN CHIEF
U.S. ATLANTIC FLEET
ATTN: FLT METEOROLOGIST
NORFOLK, VA 23511

COMMANDER IN CHIEF
U.S. ATLANTIC FLEET
ATTN: NSAP SCIENCE ADVISOR
NORFOLK, VA 23511

COMMANDER IN CHIEF
U.S. PACIFIC FLEET
CODE 02M
PEARL HARBOR, HI 96860-7000

COMMANDER IN CHIEF
U.S. NAVAL FORCES, EUROPE
ATTN: METEOROLOGICAL OFFICER
FPO NEW YORK 09510

CINCUSNAVEUR
ATTN: NSAP SCIENCE ADVISOR
BOX 100
FPO NEW YORK 09510

COMMANDER SECOND FLEET
ATTN: METEOROLOGICAL OFFICER
FPO NEW YORK 09501-6000

COMSECONDFLT
ATTN: NSAP SCIENCE ADVISOR
FPO NEW YORK 09501-6000

COMTHIRDFLT
ATTN: FLT METEOROLOGIST
PEARL HARBOR, HI 96860-7500

COMSEVENTHFLT
ATTN: FLT METEOROLOGIST
FPO SAN FRANCISCO 96601-6003

COMTHIRDFLT
ATTN: NSAP SCIENCE ADVISOR
PEARL HARBOR, HI 96860-7500

COMSEVENTHFLT
ATTN: NSAP SCIENCE ADVISOR
BOX 167
FPO SEATTLE 98762

COMSIXTHFLT
ATTN: FLT METEOROLOGIST
FPO NEW YORK 09501-6002

COMSIXTHFLT/COMFAIRMED
ATTN: NSAP SCIENCE ADVISOR
FPO NEW YORK 09501-6002

COMNAVSURFLANT
ATTN: NSAP SCIENCE ADVISOR
NORFOLK, VA 23511

COMNAVSURFPAC
(005/N6N)
ATTN: NSAP SCIENCE ADVISOR
SAN DIEGO, CA 92155-5035

COMMANDER
AMPHIBIOUS GROUP 2
ATTN: METEOROLOGICAL OFFICER
FPO NEW YORK 09501-6007

COMMANDER
AMPHIBIOUS GROUP 1
ATTN: METEOROLOGICAL OFFICER
FPO SAN FRANCISCO 96601-6006

COMMANDER
OPTEVFOR
NAVAL BASE
NORFOLK, VA 23511-6388

COMMANDER
OPTEVFOR
ATTN: NSAP SCIENCE ADVISOR
NORFOLK, VA 23511-6388

DEPUTY COMMANDER
OPTEVFOR, PACIFIC
NAS, NORTH ISLAND
SAN DIEGO, CA 92135-5000

OFFICER IN CHARGE
OPTEVFOR, SUNNYVALE
NAVAL AIR STATION
MOFFETT FIELD, CA 94035-5011

COMMANDING OFFICER
USS AMERICA (CV-66)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09531-2790

COMMANDING OFFICER
USS CORAL SEA (CV-43)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09550-2720

COMMANDING OFFICER
USS D. D. EISENHOWER (CVN-69)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09532-2830

COMMANDING OFFICER
USS FORRESTAL (CV-59)
ATTN: MET. OFFICER, OA DIV.
FPO MIAMI 34080-2730

COMMANDING OFFICER
USS INDEPENDENCE (CV-62)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09537-2760

COMMANDING OFFICER
USS J. F. KENNEDY (CV-67)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09538-2800

COMMANDING OFFICER
USS NIMITZ (CVN-68)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09542-2820

COMMANDING OFFICER
USS SARATOGA (CV-60)
ATTN: MET. OFFICER, OA DIV.
FPO MIAMI 34078-2740

PCO
USS T. ROOSEVELT (CVN-71)
ATTN: OPS OA
NEWPORT NEWS, VA 23607

COMMANDING OFFICER
USS CONSTELLATION (CV-64)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96635-2780

COMMANDING OFFICER
USS ENTERPRISE (CVN-65)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96636-2810

COMMANDING OFFICER
USS KITTY HAWK (CV-63)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96634-2770

COMMANDING OFFICER
USS MIDWAY (CV-41)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96631-2710

COMMANDING OFFICER
USS RANGER (CV-61)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96633-2750

COMMANDING OFFICER
USS CARL VINSON (CVN-70)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96629-2840

COMMANDING OFFICER
USS IOWA (BB-61)
ATTN: MET. OFFICER, OA DIV.
FPO NEW YORK 09546-1100

COMMANDING OFFICER
USS NEW JERSEY (BB-62)
ATTN: MET. OFFICER, OA DIV.
FPO SAN FRANCISCO 96688-1110

COMMANDING OFFICER
USS BLUERIDGE (LCC-19)
ATTN: MET. OFFICER
FPO SAN FRANCISCO 96628-3300

COMMANDING OFFICER
USS GUADALCANAL (LPH-7)
ATTN: MET. OFFICER
FPO NEW YORK 09562-1635

COMMANDING OFFICER
USS GUAM (LPH-9)
ATTN: MET. OFFICER
FPO NEW YORK 09563-1640

COMMANDING OFFICER
USS INCHO' (LPH-12)
ATTN: MET. OFFICER
FPO NEW YORK 09529-1655

COMMANDING OFFICER
USS IWO JIMA (LPH-2)
ATTN: MET. OFFICER
FPO NEW YORK 09561-1625

COMMANDING OFFICER
USS NASSAU (LHA-4)
ATTN: MET. OFFICER
FPO NEW YORK 09557-1615

COMMANDING OFFICER
USS SAIPAN (LHA-2)
ATTN: MET. OFFICER
FPO NEW YORK 09549-1605

COMMANDING OFFICER
USS BELLEAU WOOD (LHA-3)
ATTN: METEOROLOGICAL OFFICER
FPO SAN FRANCISCO 96623-1610

COMMANDING OFFICER
USS NEW ORLEANS (LPH-11)
ATTN: MET. OFFICER
FPO SAN FRANCISCO 96627-1650

COMMANDING OFFICER
USS OKINAWA (LPH-3)
ATTN: MET. OFFICER
FPO SAN FRANCISCO 96625-1630

COMMANDING OFFICER USS PELELIU (LHA-5) ATTN: MET. OFFICER FPO SAN FRANCISCO 96624-1620	COMMANDING OFFICER USS TARAWA (LHA-1) ATTN: MET. OFFICER FPO SAN FRANCISCO 96622-1600	COMMANDING OFFICER USS TRIPOLI (LPH-10) ATTN: METEOROLOGICAL OFFICER FPO SAN FRANCISCO 96626-1645
COMFLTAIR, MEDITERRANEAN ATTN: NSAP SCIENCE ADVISOR CODE 03A FPO NEW YORK 09521	ASST. FOR ENV. SCIENCES ASST. SEC. OF THE NAVY (R&D) ROOM 5E731, THE PENTAGON WASHINGTON, DC 20350	CHIEF OF NAVAL RESEARCH (2) LIBRARY SERVICES, CODE 784 BALLSTON TOWER #1 800 QUINCY ST. ARLINGTON, VA 22217-5000
OFFICE OF NAVAL TECHNOLOGY MAT-0724, NAVY DEPT. 800 N. QUINCY ST. ARLINGTON, VA 22217	CHIEF, ENV. SVCS. DIV. OJCS (J-33) RM. 2877K, THE PENTAGON WASHINGTON, DC 20301	ENVIRONMENTAL SERVICES DIV. OFFICE OF THE JOINT CHIEFS OF STAFF THE PENTAGON WASHINGTON, DC 20301
NAVAL DEPUTY TO THE ADMINISTRATOR, NOAA ROOM 200, PAGE BLDG. #1 3300 WHITEHAVEN ST. NW WASHINGTON, DC 20235	COMMANDING OFFICER NAVAL RESEARCH LAB ATTN: LIBRARY, CODE 2620 WASHINGTON, DC 20390	OFFICE OF NAVAL RESEARCH SCRIPPS INSTITUTION OF OCEANOGRAPHY LA JOLLA, CA 92037
COMMANDING OFFICER NAVAL OCEAN RSCH & DEV ACT NSTL, MS 39529-5004	COMMANDER NAVAL OCEANOGRAPHY COMMAND NSTL, MS 39529-5000	COMNAVOCANCOM ATTN: LCDR F. MCNAB, CODE 5311 NSTL, MS 39529-5000
COMMANDING OFFICER NAVAL OCEANOGRAPHIC OFFICE BAY ST. LOUIS NSTL, MS 39522-5001	SUPERINTENDENT LIBRARY REPORTS U.S. NAVAL ACADEMY ANNAPOULIS, MD 21402	DIRECTOR OF RESEARCH U.S. NAVAL ACADEMY ANNAPOULIS, MD 21402
NAVAL POSTGRADUATE SCHOOL METEOROLOGY DEPT. MONTEREY, CA 93943-5000	NAVAL POSTGRADUATE SCHOOL OCEANOGRAPHY DEPT. MONTEREY, CA 93943-5000	NAVAL POSTGRADUATE SCHOOL PHYSICS & CHEMISTRY DEPT. MONTEREY, CA 93943-5000
LIBRARY NAVAL POSTGRADUATE SCHOOL MONTEREY, CA 93943-5002	NAVAL POSTGRADUATE SCHOOL MATHEMATICS DEPT. MONTEREY, CA 93943-5000	COMMANDER NAVAIRSYSCOM (AIR-330) WASHINGTON, DC 20361-0001

COMMANDER, SPACE & NAVAL
WARFARE SYSTEMS COMMAND
ATTN: CAPT. K. VAN SICKLE
CODE 06G, NAVY DEPT.
WASHINGTON, DC 20363-5100

COMMANDER
NAVAL SHIP RSCH & DEV. CENTER
CODE 5220
BETHESDA, MD 20084

COMMANDER
NAVAL SURFACE WEAPONS CENTER
ATTN: CODE 44
DAHLGREN, VA 22448-5000

DIRECTOR, TECH. INFORMATION
DEFENSE ADV. RSCH PROJECTS
1400 WILSON BLVD.
ARLINGTON, VA 22209

CHIEF
MARINE & EARTH SCI. LIBRARY
NOAA, DEPT. OF COMMERCE
ROCKVILLE, MD 20852

DIRECTOR
GEOPHYS. FLUID DYNAMICS LAB
NOAA, PRINCETON UNIVERSITY
P.O. BOX 308
PRINCETON, NJ 08540

MARINE OBS. PROGRAM LEADER
ATTN: J. W. NICKERSON
NWS/NOAA, GRAMAX BLDG.
8060 13TH ST.
SILVER SPRING, MD 20910

LABORATORY FOR ATMOS. SCI.
NASA GODDARD SPACE FLIGHT CEN.
GREENBELT, MD 20771

COMMANDER
NAVOCEANSYSCEN
DR. J. RICHTER, CODE 54
SAN DIEGO, CA 92152-5000

COMMANDER
NAVAL SURFACE WEAPONS CENTER
DAHLGREN, VA 22448-5000

COMMANDING OFFICER
U.S. ARMY RESEARCH OFFICE
ATTN: GEOPHYSICS DIV.
P.O. BOX 12211
RESEARCH TRIANGLE PARK, NC
27709

COMMANDING OFFICER
USCG RSCH & DEV. CENTER
GROTON, CT 06340

NATIONAL WEATHER SERVICE
WORLD WEATHER BLDG., RM 307
5200 AUTH ROAD
CAMP SPRINGS, MD 20023

DIRECTOR
TECHNIQUES DEVELOPMENT LAB
GRAMAX BLDG.
8060 13TH ST.
SILVER SPRING, MD 20910

DR. JAMES E. OVERLAND
PACIFIC MARINE ENVIRONMENTAL
LABORATORY/NOAA
7600 SANDPOINT WAY, NE
SEATTLE, WA 98115

EXECUTIVE SECRETARY, CAO
SUBCOMMITTEE ON ATMOS. SCI.
NATIONAL SCIENCE FOUNDATION
RM. 510, 1800 G. STREET, NW
WASHINGTON, DC 20550

COMMANDER
NAVAL WEAPONS CENTER
DR. A. SHLANTA, CODE 3331
CHINA LAKE, CA 93555-6001

DIRECTOR
NAVSURFWEACEN, WHITE OAKS
NAVY SCIENCE ASSIST. PROGRAM
SILVER SPRING, MD 20910

DIRECTOR (12)
DEFENSE TECH. INFORMATION
CENTER, CAMERON STATION
ALEXANDRIA, VA 22314

DIRECTOR
NATIONAL METEORO. CENTER
NWS, NOAA
WNB W32, RM 204
WASHINGTON, DC 20233

DIRECTOR, ATLANTIC OCEANO. &
METEOROLOGY LABS
15 RICKENBACKER CAUSEWAY
VIRGINIA KEY
MIAMI, FL 33149

DIRECTOR
NATIONAL WEATHER SERVICE
GRAMAX BLDG.
8060 13TH ST.
SILVER SPRING, MD 20910

HEAD, ATMOS. SCIENCES DIV.
NATIONAL SCIENCE FOUNDATION
1800 G STREET, NW
WASHINGTON, DC 20550

DR. MARVIN DICKERSON
L-202, LLNL
P.O. BOX 808
LIVERMORE, CA 94550

ARVIN/CALSPAN ADVANCED TECH.
CENTER
ATMOS. SCI./ENV. SCI. DEPT.
P.O. BOX 400
BUFFALO, NY 14225

THE EXECUTIVE DIRECTOR
AMERICAN METEORO. SOCIETY
45 BEACON ST.
BOSTON, MA 02108

AMERICAN METECRO. SOCIETY
METEOR. & GEOASTRO. ABSTRACTS
P.O. BOX 1736
WASHINGTON, DC 20013

DIRECTOR, JTWC
BOX 17
FPO SAN FRANCISCO 96630

LIBRARY, AUSTRALIAN NUMERICAL
METEOROLOGY RESEARCH CENTER
P.O. BOX 5089A
MELBOURNE, VICTORIA, 3001
AUSTRALIA

INSTITUT FOR TEORETISK
METEOROLOGI
HARALDSGADE 6
DK-2200 KOBENHAVN N
DENMARK

DIRECTOR OF NAVAL
OCEANO. & METEOROLOGY
MINISTRY OF DEFENCE
OLD WAR OFFICE BLDG.
LONDON, S.W.1. ENGLAND

METEORO. OFFICE LIBRARY
LONDON ROAD
BRACKNELL, BERKSHIRE
RG 12 1SZ, ENGLAND

MINISTRY OF DEFENCE
NAVY DEPARTMENT
ADMIRALTY RESEARCH LAB
TEDDINGTON, MIDDX
ENGLAND

EUROPEAN CENTRE FOR MEDIUM
RANGE WEATHER FORECASTS
SHINFIELD PARK, READING
BERKSHIRE RG29AX, ENGLAND

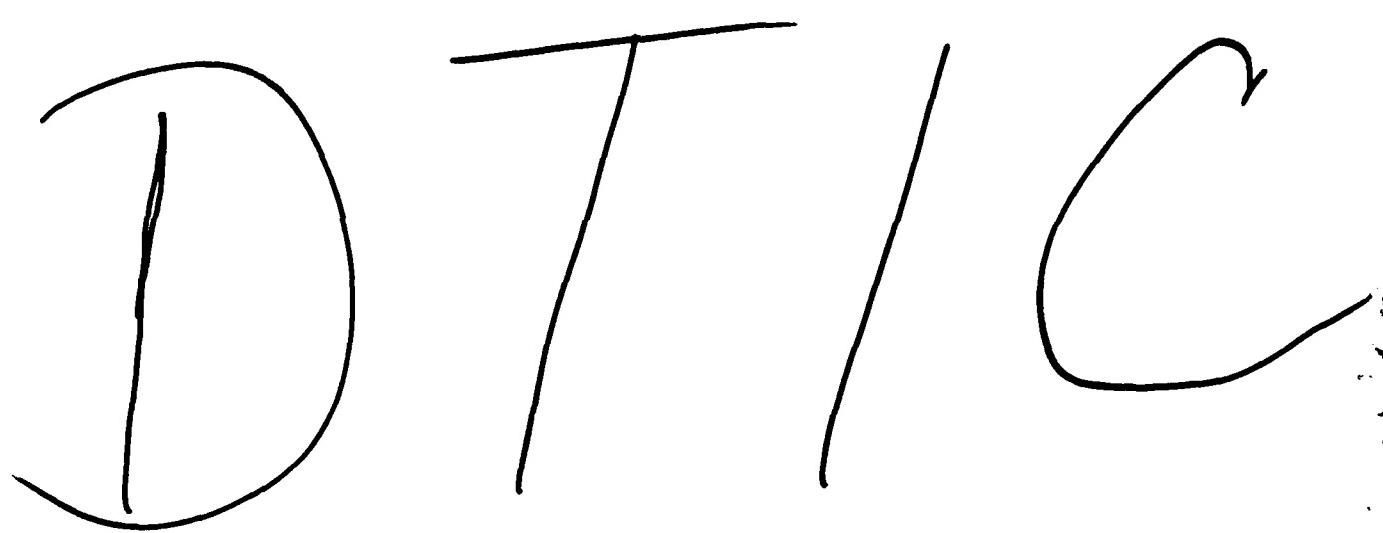
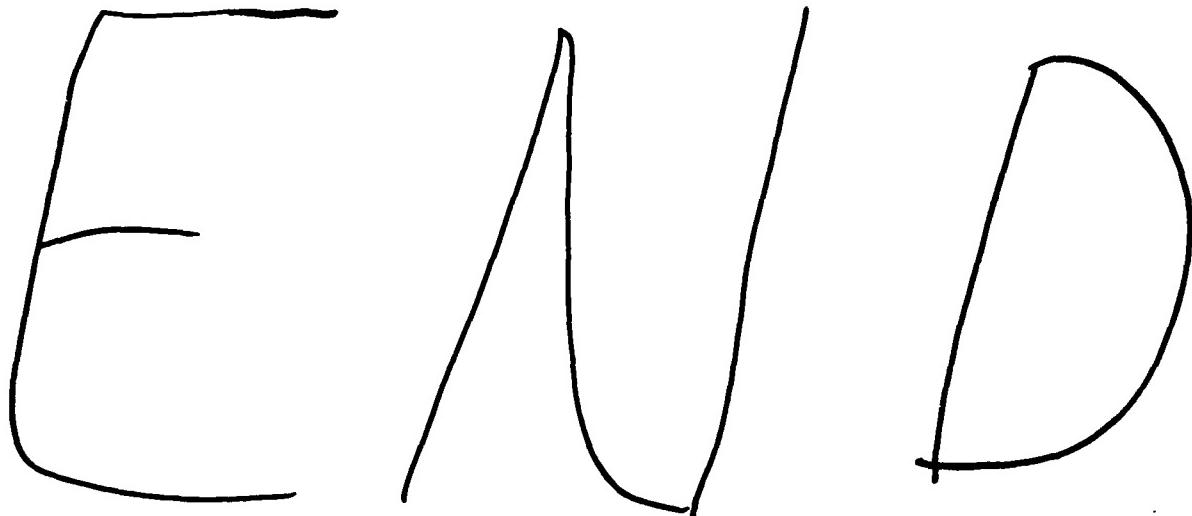
LIBRARY
FINNISH METEORO. INSTI.
BOX 503
SF-00101 HELSINKI 10
FINLAND

SERVICE HYDROGRAPHIQUE ET
OCEANOGRAPHIQUE DE LA MARINE
ESTABLISSEMENT PRINCIPAL
RUE DU CHATELLIER, B.P. 426
29275 - BREST CEDEX, FRANCE

BIBLIOTHEK DES DEUTSCHEN
WETTERDIENSTES
D 6050 OFFENBACH
POSTFACH 196
FEDERAL REPUBLIC OF GERMANY

HEAD, DATA PROCESSING SEC.
GERMAN MILITARY GEOPHYS.
MONT-ROYAL, D5580
TRAVEN-TRARBACH
FEDERAL REPUBLIC OF GERMANY

MARITIME METEOROLOGY DIV.
JAPAN METEOROLOGICAL AGENCY
OTE-MACHI 1-3-4 CHIYODA-KU
TOKYO, JAPAN



8 - 86